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AN-9091

针对PFC SPM®系列的升压PFC电感设计指南

系统结构

图 1中的原理框图显示的是用于升压功率因数校正 (PFC) 拓扑的PFC SPM® 3系列版本2 (FPAB20BH60B)。 电感(L) 在升压PFC SPM评估板上FPAB20BH60B 器件的引脚24和引脚25之间。 要达到功率因数校正的目的,电感设计至关重要。应当在不增加系统成本的情况下优化设计以通过谐波准则。 表 1显示的是待测FPAB20BH60B 评估板的典型工作条件。

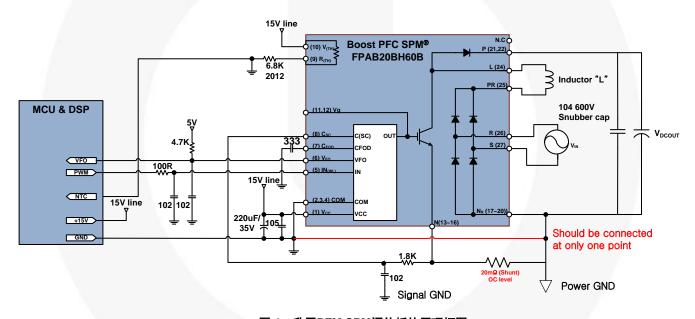


图 1. 升压PFM SPM评估板的原理框图

表 1. 典型工作条件

编号	项目	符号	数值	单位
1	开关频率	f	22	kHz
2	正常输入电压	V _{IN}	220	V_{RMS}
3	输出最大功率	Po	2200	W
4	标称输出电压	$V_{ exttt{DCOUT}}$	390	V _{DC}

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电感L的计算

下列等式用于计算电感值(L)。它根据交流输入和直流链路电压之间的电感纹波电流而得。请参见AN-42047。

$$\Delta I_{LP_{-P}} = \frac{V_{N} \left(V_{OUTDC} - V_{N} \right)}{fL V_{OUTDC}}, < \frac{V_{OUTDC}}{V_{N}} = \frac{1}{1 - D},$$

$$\Delta I_{LP_{-P}} = \frac{V_{N} * D * T}{L}$$

$$(1)$$

其中:

 ΔI_{LP-P} : PFC电感电流峰峰值;

V_{IN}: 输入交流电压(V_{RMS});

V_{outbc}: 直流链路电压(V);

f: 开关频率(Hz); 和

L: PFC电感值(H)。

$$\Delta I_{LP_P} = \frac{V_N (V_{OUTDC} - V_N)}{fL V_{OUTDC}}$$

$$\therefore (\Delta I_{LP_P})_{MAX} = \frac{V_{OUTDC}}{4fL}, \therefore V_N = \frac{1}{2} V_{OUTDC}$$
(2)

假设f=22 kHz, V_{0UTDC}=390 V_{DC}, ΔI_{LP_P}=4.0 A, 则可按下式计算电感L:

$$L = V_{OUTDC} / (4 \times f \times \Delta I_{LP_P}) = 390 V_{DC} / (4 \times 22kHz \times 4.0A) = 1.108mH$$
 (3)

选择导线直径

在表

1的工作条件下, 额定输出功率为2.4 kW, 交流输入的 额定电压为220 V_{Ac}。最大输入电流可由下式获得:

$$I_{AC_MAX} = 2.2kW/220V_{AC} = 10.0Arms$$
 (4)

假设每平方mm铜线的rms电流为5 [Arms/mm²],则导线面积和直径可由下式计算得出:

$$Aw = I_{AC_MAX} / (5[A/mm^2])$$

= 10.0 Arms (5[A/mm^2]) = 2.0 mm²]

Radius of wire = SQRT(Aw/3.14)= SQRT(2.0/3.14) = 0.80[mm]

因此,选择直径为2.0 mm的铜线。

磁芯选择

选择磁芯时,需考虑很多因素:

磁芯材料、磁芯磁导率、有效横截面积(cm²)、磁路长度(cm)和标称电感(nH/N²)。出于性能方面的考虑,选用Mega Flux®磁芯。

Magnetic PathLengthI = 18.38cm = 183.8mm (8)

Cross Section Area A (9)

 $=5.04cm^2=183.8mm$

Initialpermeability u =

 $60 \times 4 \times 3.14 \times 1e - 10(H/mm)$ at 25kHz (10)

材料特性

- 化学成分: 铁硅合金
- 饱和通量密度 16.000 高斯
- 居里温度: 550°C
- 初始磁导率:

60 μ ±12%, 测量条件: 25 kHz、1 V和0 A_{直流}

尺寸 磁尺寸

- 磁路长度: 18.38 cm
- 横截面积: 5.04 cm²

物理尺寸 (壳体)

- 外径: 79.50 sm (最大值)
- 内径: 41.14 cm (最小值)
- 高度: 55.0 cm (最大值)

壳体

(5)

(6)

- 成分: PBT (POLY BUTHYLENE TERPHTALATE)
- 制造商: KOLON
- UL阻燃等级和文件编号: UL 94-V0, E88499

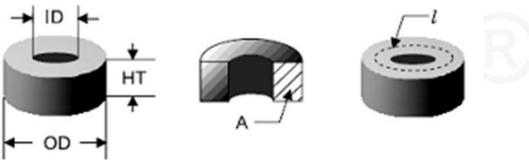
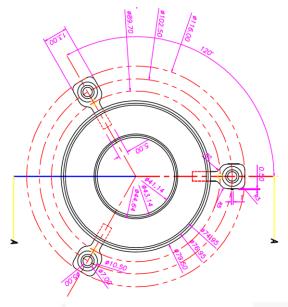


图 2. 所选环形芯的规格: CK740060C



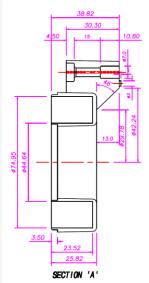


图 3. 磁芯壳体尺寸

线路匝数计算

图 4显示带环形芯的升压PFC电感及其走线。

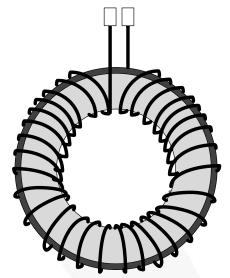


图 4. 带 环形芯 的升压PFC SPM电感走线

对于电感而言,可通过下式计算其每条导线的匝数(N),参考网站: http://www.changsung.com:

$$L = \frac{0.4\pi\mu N^2 A * 10^{-2}}{1} \tag{11}$$

根据等式(8)

(10)和(11)中的磁芯参数,可如下计算N:

$$N = SQRT(1.108mH \times 183.9/(60 \times 4 \times 3.14 \times 1e - 10/H \times 504) = 74turn$$
(12)

因此,所选匝数应大于计算得到的74匝。选择导线的74 匝作为升压PFC SPM®电感的最终匝数。

AN-9091 应用氧

PFC电感的实施



图 5. 电感俯视图



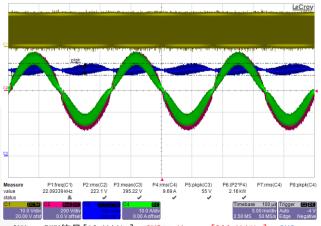
图 6. 铜线宽度(2.01 mm)



图 7. 电感值(0.98 mH)

根据计算,选定的铜线宽2.0 mm, 电感值为1.1 mH。实际值为:铜线宽2.01 mm, 电感0.98 mH。

通过测试验证设计



CH1: PWM信号[10 V/div], CH2: V_{AC_INPUT} [200 V/div], CH3: V_∞电压[100 V/div], CH4: 电感电流[10 A/div]

图 8. 满载测试结果(9.69 Arms)

经验证,电感电流的最大纹波电流大于4A $p_{K,PK}$, 与等式中 $\Delta_{IRP,F}$ (3)的假设值相近。

参考文献

AN-42047 — 功率因数校正 (PFC) 基础知识AN-6982 — 采用FAN6982的功率因数校正转换器设计磁粉芯: http://www.changsung.com/

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